

**DRAIN STUDY**  
**LINCOLN MEADOWS**

City of Lincoln, California  
November 23, 2015

Prepared by:

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I. Introduction

The proposed Lincoln Meadows subdivision will divide 40 acres into 148 low density single family homes. The purpose of this report is to determine the runoff generated by development of the subdivision and the pipe system to convey the runoff to the outfalls.

Location

The Lincoln Meadows project is located on the northwest corner of the intersection of Virginatown Road and Hungry Hollow Road, in the City of Lincoln (See Figure 1).

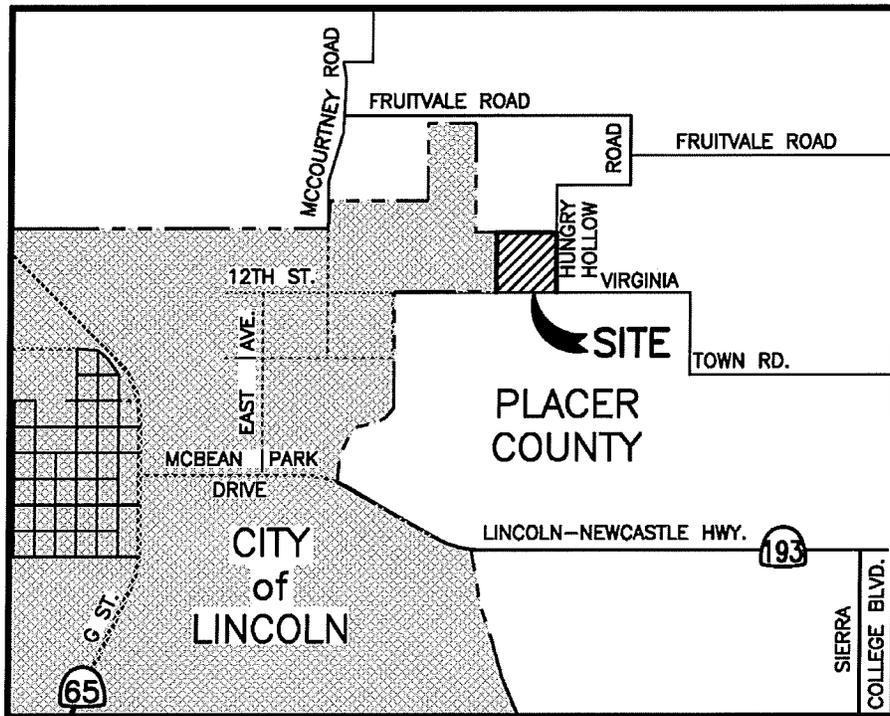


Figure 1 - Vicinity Map

II. Narrative

The Lincoln Meadows project drains into two watersheds; the north portion of the project drains to Markham Ravine and the south portion drains to Auburn Ravine. Lincoln Meadows will be developed according to the City of Lincoln Design Criteria and Procedures Manual. Low Impact Development (LID) measures will be implemented to provide infiltration and evaporation opportunities for the runoff, which will reduce the flows into the drain system and help mitigate increased flows due to development. Two

detention basins will be built to maintain the post-project flows at 90% of the pre-project flows, one for each watershed, and will be sized to treat the remaining runoff from the impervious area that has not been treated by the LID measures.

### III. Runoff and Flow Projections

The design flow was determined by using the City of Lincoln Design Criteria and Procedures Manual, Section 10-7. The spreadsheet for the drain pipe calculations was also developed from procedures outlined in Section 10-7. The Preliminary Drainage Study Exhibit depicts all of the sheds and pipe sizes comprising the proposed drain system, this exhibit is included in Appendix 'A' and the calculation spreadsheet is in Appendix 'B'.

LID measures will be installed in Lincoln Meadows to reduce the runoff from impervious surfaces. These measures include: disconnected roof drains, interceptor trees, and detached sidewalk.

The runoff reduction worksheet Form D-1e calculates the Water Quality Flow (WQF) created by the project. This worksheet was developed for Sacramento, Roseville and Folsom, but since the site has minimal clay soil and the rainfall intensity is similar to that in Roseville, this worksheet can be used to determine the runoff reduction for Lincoln Meadows. The WQF is generated by the 2 year or less "first flush" storm. The formula to calculate this flow is  $WQF = ciA$ , where  $c$  is the runoff coefficient,  $i$  is the rainfall intensity and  $A$  is the adjusted area for treatment, which is reduced due to the LID measures being incorporated into the project. Volume based treatment provided by the detention basins is proposed for Lincoln Meadows, Roseville uses the CASQA volume calculation.

The north and south watersheds each have a Form D-1e worksheet and these have been included in Appendix 'C'.

The two detention basins that will provide flow attenuation and water treatment are currently being designed by West Yost Associates and will be included in Appendix 'D' when available.

### IV. Drain System

Lincoln Meadows will construct a storm drain system; the location of the storm drain system will be five feet north or west of the street centerline, as specified in the City of Lincoln Design Criteria and Procedures Manual, Section 10-5. The drain system will be sized to carry the 10 year storm, as specified in the City of Lincoln Design Criteria and Procedures Manual, Section 10-6, pipe sizes vary from 12" diameter to 30" diameter. The flow from larger storm events will travel overland in the streets to outfall points into Lot A; the allowable street encroachments specified in Table 10-1 will be maintained. All lot grading will be designed to have a minimum of one foot of freeboard above the 100 year water surface elevation.

V. Project Phasing

The Lincoln Meadows project is proposed to be broken up in two phases: Phase 1 building 76 lots and Phase 2 building the remaining 72 lots. While phasing is anticipated, this report analyzes the entire project being completely built out.

VI. Conclusions

The development of the Lincoln Meadows will be done utilizing practices and construction methods that will prevent impacting the existing flows and water quality of the Auburn Ravine and Markham Ravine watersheds that will receive drainage from this project.

The development of Lincoln Meadows will be done according to the City of Lincoln Design Criteria and Procedures Manual Chapter 10 which specifies how to design drainage systems.

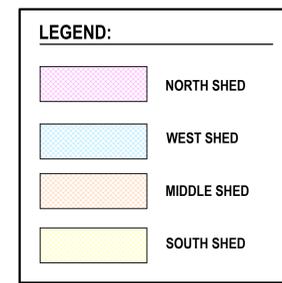
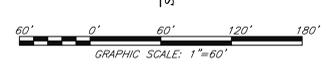
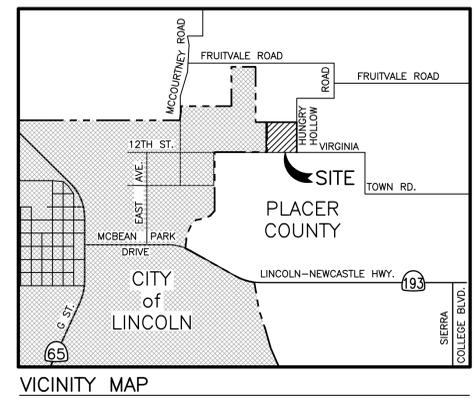
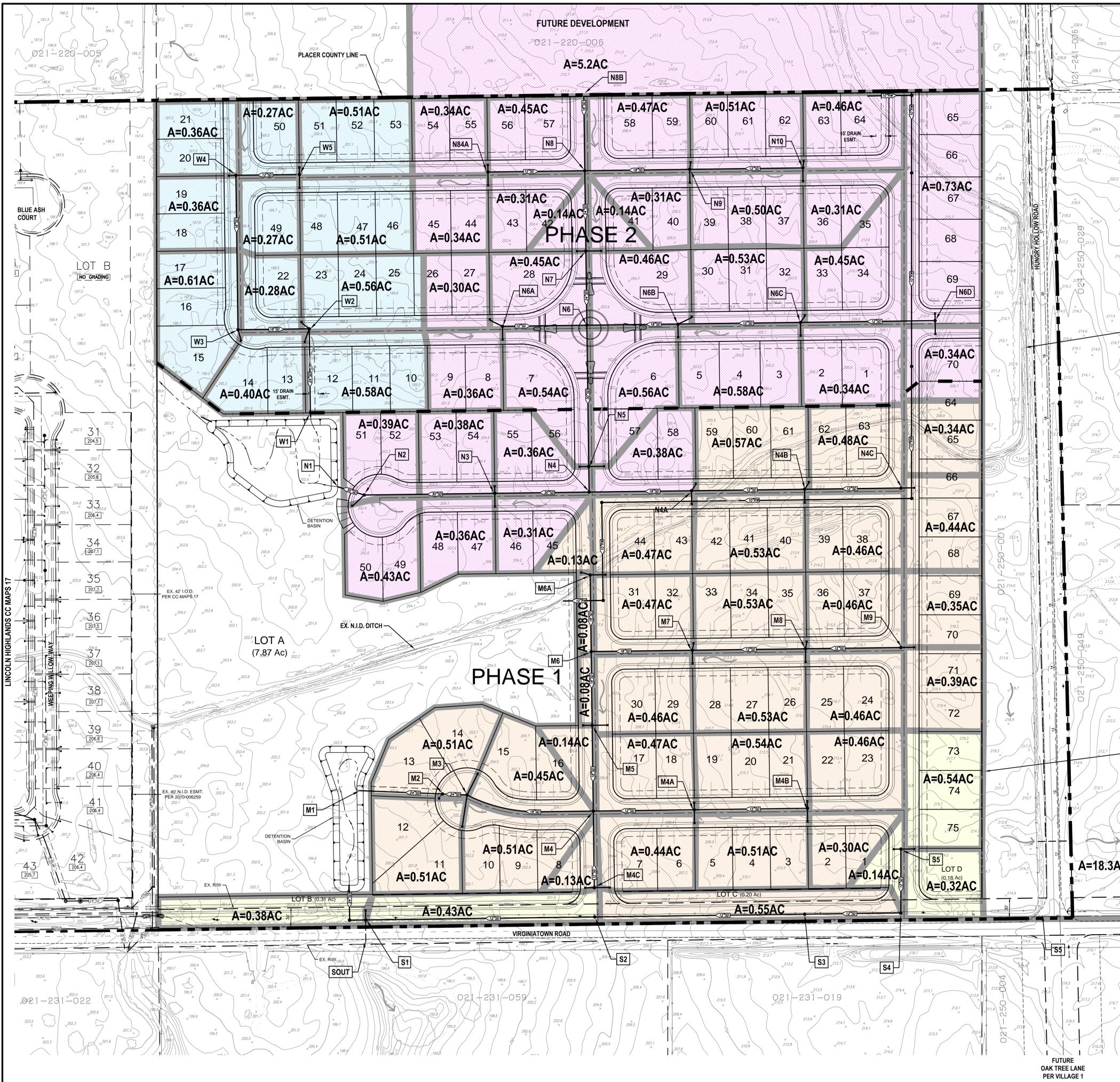
LID measures such as disconnected roof drains, interceptor tree planting and detached sidewalks will be used to reduce the runoff that increases from the impervious surfaces constructed with development.

Peak flow increases will be mitigated by the construction of two detention basins, one for each of the watersheds existing on the property.

A Storm Water Pollution Prevention Program (SWPPP) will be developed for Lincoln Meadows and it will include an erosion control plan that indicates where Best Management Practices (BMP) measures will be implemented during construction to prevent soil and pollutants from entering the watersheds.

**APPENDIX A**

Preliminary Drainage Study Exhibit



**PRELIMINARY DRAINAGE STUDY**  
**LINCOLN MEADOWS**  
 CITY OF LINCOLN - PLACER COUNTY - CALIFORNIA  
 OCTOBER 19, 2015  
 SCALE: 1"=60'  
 BAKER-WILLIAMS ENGINEERING GROUP

**BW** BAKER-WILLIAMS ENGINEERING GROUP  
 Engineering / Surveying / Land Planning / Entitlement Processing / GPS Services  
 6020 Rutland Drive, Suite 19 ~ Carmichael CA 95608  
 (916) 331-4336 ~ fax (916) 331-4430 ~ office@bwengineers.com

S:\BMEG Jobs\2015\Lincoln Meadows\Engineering\Drawings\0301016.PREL-Drain Study.dwg - Sheet 1 - 10/19/2015 2:20:23 PM - R10406.Ea

0301016-PREL-DRAIN STUDY

**APPENDIX B**

Calculation Spreadsheet

LINCOLN MEADOW PRELIMINARY DRAINAGE CALCULATIONS

| NODE        | TO  | FROM                 | AREA<br>(acres) | CUM<br>AREA | *Tr<br>overland<br>(min) | **Tr<br>collector<br>(min) | V<br>(ft/s) | L<br>(ft) | Tr<br>conduit<br>(min) | Total<br>Response<br>(min) | q <sub>10</sub> | q <sub>25</sub> | q <sub>100</sub> | Fi  | 50%AP | FiAp | Qp <sub>10</sub> =<br>q <sub>10</sub> A-FiAp | Qp <sub>25</sub> =<br>q <sub>25</sub> A-FiAp | Qp <sub>100</sub> =<br>q <sub>100</sub> A-FiAp | STORM DRAIN PIPE |        |     |       |     | 10 yr HYD GRADE LINE |        |     |          |          |  |  |
|-------------|-----|----------------------|-----------------|-------------|--------------------------|----------------------------|-------------|-----------|------------------------|----------------------------|-----------------|-----------------|------------------|-----|-------|------|--|--|--|------------------|--------|-----|-------|-----|----------------------|--------|-----|----------|----------|--|--|
|             |     |                      |                 |             |                          |                            |             |           |                        |                            |                 |                 |                  |     |       |      |  |  |  | DIA              | SLOPE  | L   | Qmax  | VEL | n                    | SLOPE  | RIM | UPPER MH | LOWER MH |  |  |
| NORTH SHED  |     |                      |                 |             |                          |                            |             |           |                        |                            |                 |                 |                  |     |       |      |  |  |  |                  |        |     |       |     |                      |        |     |          |          |  |  |
| DI-N10N     | N10 | OVERLAND             | 0.46            | 0.46        | 15.00                    | 5.68                       | 2.8         | 12        | 0.07                   | 20.7                       | 1.28            | 1.66            | 2.04             | 0.2 | 0.23  | 0.0  | 0.54   | 0.72   | 0.89   | 12               | 0.0050 | 12  | 2.19  | 2.8 | 0.015                | 0.0003 |     |          |          |  |  |
| DI-N10S     | N10 | OVERLAND             | 0.31            | 0.31        | 15.00                    | 5.24                       | 2.8         | 24        | 0.14                   | 20.2                       | 1.30            | 1.68            | 2.06             | 0.2 | 0.16  | 0.0  | 0.37   | 0.49   | 0.61   | 12               | 0.0050 | 24  | 2.19  | 2.8 | 0.015                | 0.0001 |     |          |          |  |  |
| N10         | N9  | DI-N10N&DI-N10S      | 0.00            | 0.77        |                          |                            | 6.8         | 180       | 0.44                   | 20.4                       | 1.29            | 1.67            | 2.06             | 0.2 | 0.39  | 0.1  | 0.92   | 1.21   | 1.51   | 12               | 0.0300 | 180 | 5.36  | 6.8 | 0.015                | 0.0009 |     |          |          |  |  |
| N9          | N8  | N10, DI-N9N&DI-N9S   | 1.79            | 2.56        |                          |                            | 2.3         | 160       | 1.16                   | 20.8                       | 1.27            | 1.65            | 2.03             | 0.2 | 1.28  | 0.3  | 2.99   | 3.97   | 4.95   | 18               | 0.0020 | 160 | 4.08  | 2.3 | 0.015                | 0.0011 |     |          |          |  |  |
| N8          | N7  | N9, N8A&N8B          | 0.00            | 9.20        |                          |                            | 3.7         | 130       | 0.59                   | 22.0                       | 1.21            | 1.61            | 1.98             | 0.2 | 4.60  | 0.9  | 10.21  | 13.87  | 17.29  | 24               | 0.0035 | 130 | 11.62 | 3.7 | 0.015                | 0.0027 |     |          |          |  |  |
| N7          | N6  | N8, DI-N7E&DI-N7W    | 0.28            | 9.48        |                          |                            | 3.7         | 120       | 0.54                   | 22.6                       | 1.18            | 1.59            | 1.95             | 0.2 | 4.74  | 0.9  | 10.26  | 14.10  | 17.57  | 24               | 0.0035 | 120 | 11.62 | 3.7 | 0.015                | 0.0027 |     |          |          |  |  |
| N6          | N5  | N7, N6A&N6B          | 0.00            | 14.02       |                          |                            | 3.6         | 215       | 0.99                   | 23.1                       | 1.16            | 1.57            | 1.93             | 0.2 | 7.01  | 1.4  | 14.84  | 20.59  | 25.66  | 30               | 0.0025 | 215 | 17.81 | 3.6 | 0.015                | 0.0017 |     |          |          |  |  |
| N5          | N4  | N6, DI-N5E&DI-N5W    | 1.48            | 15.50       |                          |                            | 3.6         | 40        | 0.18                   | 24.1                       | 1.12            | 1.54            | 1.89             | 0.2 | 7.75  | 1.6  | 15.76  | 22.25  | 27.75  | 30               | 0.0025 | 40  | 17.81 | 3.6 | 0.015                | 0.0020 |     |          |          |  |  |
| N4          | N3  | N5&N4A               | 0.00            | 18.32       |                          |                            | 4.3         | 150       | 0.58                   | 24.3                       | 1.11            | 1.53            | 1.88             | 0.2 | 9.16  | 1.8  | 18.49  | 26.20  | 32.67  | 30               | 0.0035 | 150 | 21.08 | 4.3 | 0.015                | 0.0027 |     |          |          |  |  |
| N3          | N2  | N4, DI-N3N&DI-N3S    | 1.41            | 19.73       |                          |                            | 4.3         | 210       | 0.82                   | 24.9                       | 1.09            | 1.51            | 1.86             | 0.2 | 9.87  | 2.0  | 19.47  | 27.86  | 34.74  | 30               | 0.0035 | 210 | 21.08 | 4.3 | 0.015                | 0.0030 |     |          |          |  |  |
| N2          | N1  | N2&DI-N2S            | 0.82            | 20.55       |                          |                            | 4.3         | 40        | 0.16                   | 25.7                       | 1.06            | 1.49            | 1.83             | 0.2 | 10.28 | 2.1  | 19.66  | 28.52  | 35.57  | 30               | 0.0035 | 40  | 21.08 | 4.3 | 0.015                | 0.0031 |     |          |          |  |  |
| N1          |     |                      |                 |             |                          |                            |             |           |                        |                            |                 |                 |                  |     |       |      |  |  |  |                  |        |     |       |     |                      |        |     |          |          |  |  |
| N8B         | N8  | OFFSITE              | 5.20            | 5.20        |                          |                            |             |           |                        |                            |                 |                 |                  |     |       |      |  |  |  |                  |        |     |       |     |                      |        |     |          |          |  |  |
| N8          |     |                      |                 |             |                          |                            |             |           |                        |                            |                 |                 |                  |     |       |      |  |  |  |                  |        |     |       |     |                      |        |     |          |          |  |  |
| DI-N8AN     | N8A | OVERLAND             | 0.79            | 0.79        | 15.00                    | 9.95                       | 2.8         | 12        | 0.07                   | 25.0                       | 1.08            | 1.51            | 1.86             | 0.2 | 0.40  | 0.1  | 0.78   | 1.11   | 1.39   | 12               | 0.0050 | 12  | 2.19  | 2.8 | 0.015                | 0.0006 |     |          |          |  |  |
| DI-N8AS     | N8A | OVERLAND             | 0.65            | 0.65        | 15.00                    | 7.29                       | 2.8         | 24        | 0.14                   | 22.4                       | 1.19            | 1.59            | 1.96             | 0.2 | 0.33  | 0.1  | 0.71   | 0.97   | 1.21   | 12               | 0.0050 | 24  | 2.19  | 2.8 | 0.015                | 0.0005 |     |          |          |  |  |
| N8A         | N8  | DI-N8AN&DI-N8AS      | 0.00            | 1.44        |                          |                            | 2.8         | 155       | 0.93                   | 26.0                       | 1.05            | 1.48            | 1.82             | 0.2 | 0.72  | 0.1  | 1.36   | 1.99   | 2.48   | 12               | 0.0050 | 155 | 2.19  | 2.8 | 0.015                | 0.0020 |     |          |          |  |  |
| N8          |     |                      |                 |             |                          |                            |             |           |                        |                            |                 |                 |                  |     |       |      |  |  |  |                  |        |     |       |     |                      |        |     |          |          |  |  |
| DI-N6AN     | N6A | OVERLAND             | 0.75            | 0.75        | 15.00                    | 8.48                       | 2.8         | 12        | 0.07                   | 23.5                       | 1.14            | 1.55            | 1.91             | 0.2 | 0.38  | 0.1  | 0.78   | 1.09   | 1.36   | 12               | 0.0050 | 12  | 2.19  | 2.8 | 0.015                | 0.0006 |     |          |          |  |  |
| DI-N6AS     | N6A | OVERLAND             | 0.36            | 0.36        | 15.00                    | 8.18                       | 2.8         | 24        | 0.14                   | 23.3                       | 1.15            | 1.56            | 1.92             | 0.2 | 0.18  | 0.0  | 0.38   | 0.53   | 0.66   | 12               | 0.0050 | 24  | 2.19  | 2.8 | 0.015                | 0.0001 |     |          |          |  |  |
| N6A         | N6A | DI-N6AN&DI-N6AS      | 0.00            | 1.11        |                          |                            | 2.8         | 130       | 0.78                   | 24.3                       | 1.11            | 1.53            | 1.88             | 0.2 | 0.56  | 0.1  | 1.12   | 1.59   | 1.98   | 12               | 0.0050 | 130 | 2.19  | 2.8 | 0.015                | 0.0013 |     |          |          |  |  |
| N6          |     |                      |                 |             |                          |                            |             |           |                        |                            |                 |                 |                  |     |       |      |  |  |  |                  |        |     |       |     |                      |        |     |          |          |  |  |
| DI-N6DN     | N6D | OVERLAND             | 0.73            | 0.73        | 15.00                    | 5.24                       | 2.8         | 12        | 0.07                   | 20.3                       | 1.30            | 1.67            | 2.06             | 0.2 | 0.37  | 0.1  | 0.87   | 1.15   | 1.43   | 12               | 0.0050 | 12  | 2.19  | 2.8 | 0.015                | 0.0008 |     |          |          |  |  |
| DI-N6DS     | N6D | OVERLAND             | 0.13            | 0.34        | 15.00                    | 4.02                       | 2.8         | 24        | 0.14                   | 19.2                       | 1.32            | 1.72            | 2.12             | 0.2 | 0.17  | 0.0  | 0.42   | 0.55   | 0.69   | 12               | 0.0050 | 24  | 2.19  | 2.8 | 0.015                | 0.0002 |     |          |          |  |  |
| N6D         | N6C | DI-N6DN&DI-N6DS      | 0.00            | 1.07        |                          |                            | 2.8         | 155       | 0.93                   | 21.2                       | 1.25            | 1.64            | 2.01             | 0.2 | 0.54  | 0.1  | 1.23   | 1.64   | 2.05   | 12               | 0.0050 | 200 | 2.19  | 2.8 | 0.015                | 0.0016 |     |          |          |  |  |
| N6C         | N6B | N6D, DI-N6CN&DI-N6CS | 0.79            | 1.86        |                          |                            | 2.8         | 190       | 1.14                   | 22.4                       | 1.19            | 1.59            | 1.96             | 0.2 | 0.93  | 0.2  | 2.03   | 2.78   | 3.46   | 12               | 0.0050 | 190 | 2.19  | 2.8 | 0.015                | 0.0043 |     |          |          |  |  |
| N6B         | N6  | N6C, DI-N6BN&DI-N6BS | 1.57            | 3.43        |                          |                            | 3.6         | 140       | 0.64                   | 23.0                       | 1.16            | 1.57            | 1.93             | 0.2 | 1.72  | 0.3  | 3.64   | 5.05   | 6.29   | 18               | 0.0050 | 140 | 6.45  | 3.6 | 0.015                | 0.0016 |     |          |          |  |  |
| N6          |     |                      |                 |             |                          |                            |             |           |                        |                            |                 |                 |                  |     |       |      |  |  |  |                  |        |     |       |     |                      |        |     |          |          |  |  |
| DI-N4CE     | N4C | OVERLAND             | 0.78            | 0.78        | 15.00                    | 5.24                       | 2.8         | 12        | 0.07                   | 20.3                       | 1.30            | 1.67            | 2.06             | 0.2 | 0.39  | 0.1  | 0.93   | 1.23   | 1.53   | 12               | 0.0050 | 12  | 2.19  | 2.8 | 0.015                | 0.0009 |     |          |          |  |  |
| N4C         | N4B | DI-N4CE              | 0.00            | 0.78        |                          |                            | 2.8         | 150       | 0.90                   | 21.2                       | 1.25            | 1.64            | 2.01             | 0.2 | 0.39  | 0.1  | 0.90   | 1.20   | 1.49   | 12               | 0.0050 | 150 | 2.19  | 2.8 | 0.015                | 0.0008 |     |          |          |  |  |
| N4B         | N4A | N4C, DI-N4BN&DI-N4BS | 0.94            | 1.72        |                          |                            | 3.6         | 180       | 0.82                   | 22.0                       | 1.21            | 1.61            | 1.98             | 0.2 | 0.86  | 0.2  | 1.90   | 2.59   | 3.23   | 18               | 0.0050 | 180 | 6.45  | 3.6 | 0.015                | 0.0004 |     |          |          |  |  |
| N4A         | N4  | N4B, DI-N4AN&DI-N4AS | 1.10            | 2.82        |                          |                            | 3.6         | 160       | 0.73                   | 22.8                       | 1.17            | 1.58            | 1.94             | 0.2 | 1.41  | 0.3  | 3.03   | 4.17   | 5.20   | 18               | 0.0050 | 160 | 6.45  | 3.6 | 0.015                | 0.0011 |     |          |          |  |  |
| N4          |     |                      |                 |             |                          |                            |             |           |                        |                            |                 |                 |                  |     |       |      |  |  |  |                  |        |     |       |     |                      |        |     |          |          |  |  |
| MILDDE SHED |     |                      |                 |             |                          |                            |             |           |                        |                            |                 |                 |                  |     |       |      |  |  |  |                  |        |     |       |     |                      |        |     |          |          |  |  |
| DI-M9E      | M9  | OVERLAND             | 0.74            | 0.74        | 15.00                    | 5.24                       | 2.8         | 24        | 0.14                   | 20.2                       | 1.30            | 1.68            | 2.06             | 0.2 | 0.37  | 0.1  | 0.89   | 1.17   | 1.45   | 12               | 0.0050 | 24  | 2.19  | 2.8 | 0.015                | 0.0008 |     |          |          |  |  |
| M9          | M8  | DI-N9E               | 0.00            | 0.74        |                          |                            | 2.8         | 140       | 0.84                   | 20.4                       | 1.29            | 1.67            | 2.06             | 0.2 | 0.37  | 0.1  | 0.88   | 1.16   | 1.45   | 12               | 0.0050 | 140 | 2.19  | 2.8 | 0.015                | 0.0008 |     |          |          |  |  |
| M8          | M7  | M9, DI-M8N&DI-M8S    | 0.92            | 1.66        |                          |                            | 2.8         | 180       | 1.08                   | 21.2                       | 1.25            | 1.64            | 2.01             | 0.2 | 0.83  | 0.2  | 1.90   | 2.55   | 3.18   | 12               | 0.0050 | 180 | 2.19  | 2.8 | 0.015                | 0.0038 |     |          |          |  |  |
| M7          | M6  | M8, DI-M7N&DI-M7S    | 1.06            | 2.72        |                          |                            | 5.1         | 160       | 0.52                   | 22.3                       | 1.19            | 1.60            | 1.96             | 0.2 | 1.36  | 0.3  | 2.98   | 4.07   | 5.07   | 18               | 0.0100 | 160 | 9.12  | 5.1 | 0.015                | 0.0011 |     |          |          |  |  |
| M3          | M2  | M4, DI-M3N&DI-M3S    | 0.96            | 8.90        |                          |                            | 6.2         | 35        | 0.09                   | 24.4                       | 1.11            | 1.53            | 1.88             | 0.2 | 4.45  | 0.9  | 8.96   | 12.70  | 15.84  | 24               | 0.0100 | 35  | 19.65 | 6.2 | 0.015                | 0.0021 |     |          |          |  |  |
| M2          | M1  | M3&DI-M22            | 1.02            | 9.92        |                          |                            | 6.2         | 135       | 0.36                   | 24.5                       | 1.10            | 1.52            | 1.88             | 0.2 | 4.96  | 1.0  | 9.95   | 14.13  | 17.62  | 24               | 0.0100 | 135 | 19.65 | 6.2 | 0.015                | 0.0026 |     |          |          |  |  |
| M1          |     |                      |                 |             |                          |                            |             |           |                        |                            |                 |                 |                  |     |       |      |  |  |  |                  |        |     |       |     |                      |        |     |          |          |  |  |
| M6A         | M6  | DI-M6AE&DI-M6AW      | 1.14            | 1.14        | 15.00                    | 9.95                       | 2.8         | 125       | 0.75                   | 25.7                       | 1.06            | 1.49            | 1.83             | 0.2 | 0.57  | 0.1  | 1.09   | 1.58   | 1.97   | 12               | 0.0050 | 125 | 2.19  | 2.8 | 0.015                | 0.0012 |     |          |          |  |  |
| M6          |     |                      |                 |             |                          |                            |             |           |                        |                            |                 |                 |                  |     |       |      |  |  |  |                  |        |     |       |     |                      |        |     |          |          |  |  |
| DI-M4CE     | M4C | OVERLAND             | 0.99            | 0.99        | 15.00                    | 9.95                       | 2.8         | 12        | 0.07                   | 25.0                       | 1.08            | 1.51            | 1.86             | 0.2 | 0.50  | 0.1  | 0.97   | 1.39   | 1.74   | 12               | 0.0050 | 12  | 2.19  | 2.8 | 0.015                | 0.0010 |     |          |          |  |  |
| DI-M4CW     | M4C | OVERLAND             | 0.13            | 0.13        | 15.00                    | 7.29                       | 2.8         | 24        | 0.14                   | 22.4                       | 1.19            | 1.59            | 1.96             | 0.2 | 0.07  | 0.0  | 0.14   | 0.19   | 0.24   | 12               | 0.0050 | 24  | 2.19  | 2.8 | 0.015                | 0.0000 |     |          |          |  |  |
| M4C         | M4  | DI-M4CE&DI-M4CW      | 0.00            | 1.12        |                          |                            | 2.8         | 120       | 0.72                   | 25.7                       | 1.05            | 1.49            | 1.83             | 0.2 | 0.56  | 0.1  | 1.07   | 1.   |  |                  |        |     |       |     |                      |        |     |          |          |  |  |

LINCOLN MEADOW PRELIMINARY DRAINAGE CALCULATIONS

| NODE       | TO   | FROM                | AREA<br>(acres) | CUM<br>AREA  | *Tr<br>overland<br>(min) | **Tr<br>collector<br>(min) | V<br>(ft/s) | L<br>(ft) | Tr<br>conduit<br>(min) | Total<br>Response<br>(min) | q <sub>10</sub> | q <sub>25</sub> | q <sub>100</sub> | Fi  | 50%AP | FiAp | Qp <sub>10</sub> =<br>q <sub>10</sub> A-FiAp | Qp <sub>25</sub> =<br>q <sub>25</sub> A-FiAp | Qp <sub>100</sub> =<br>q <sub>100</sub> A-FiAp | STORM DRAIN PIPE |        |     |              |     | 10 yr HYD GRADE LINE |        |     |          |          |  |
|------------|------|---------------------|-----------------|--------------|--------------------------|----------------------------|-------------|-----------|------------------------|----------------------------|-----------------|-----------------|------------------|-----|-------|------|--|--|--|------------------|--------|-----|--------------|-----|----------------------|--------|-----|----------|----------|--|
|            |      |                     |                 |              |                          |                            |             |           |                        |                            |                 |                 |                  |     |       |      |  |  |  | DIA              | SLOPE  | L   | Qmax         | VEL | n                    | SLOPE  | RIM | UPPER MH | LOWER MH |  |
| M4B        | M4A  | DI-M4BN&DI-M4BS     | 0.00            | <b>0.76</b>  |                          |                            | 2.8         | 180       | 1.08                   | <b>21.4</b>                | 1.24            | 1.63            | 2.01             | 0.2 | 0.38  | 0.1  | <b>0.87</b>                                  | 1.16   | <b>1.45</b>                                    | 12               | 0.0050 | 180 | <b>2.19</b>  | 2.8 | 0.015                | 0.0008 |     |          |          |  |
| M4A        | M4   | M4B,DI-M4AN&DI-M4AS | 1.05            | <b>1.81</b>  |                          |                            | 2.8         | 160       | 0.96                   | <b>22.4</b>                | 1.19            | 1.59            | 1.96             | 0.2 | 0.91  | 0.2  | <b>1.98</b>                                  | 2.71   | <b>3.37</b>                                    | 12               | 0.0050 | 160 | <b>2.19</b>  | 2.8 | 0.015                | 0.0041 |     |          |          |  |
| M4         |      |                     |                 |              |                          |                            |             |           |                        |                            |                 |                 |                  |     |       |      |  |  |  |                  |        |     |              |     |                      |        |     |          |          |  |
| SOUTH SHED |      |                     |                 |              |                          |                            |             |           |                        |                            |                 |                 |                  |     |       |      |  |  |  |                  |        |     |              |     |                      |        |     |          |          |  |
| DI-S5E     | S5   | OVERLAND            | 0.86            | <b>0.86</b>  | 15.00                    | 9.95                       | 2.8         | 24        | 0.14                   | <b>25.1</b>                | 1.08            | 1.51            | 1.85             | 0.2 | 0.43  | 0.1  | <b>0.84</b>                                  | 1.21   | <b>1.51</b>                                    | 12               | 0.0050 | 24  | <b>2.19</b>  | 2.8 | 0.015                | 0.0007 |     |          |          |  |
| DI-S5S     | S5   | OVERLAND            | 0.14            | <b>0.14</b>  | 15.00                    | 7.29                       | 2.8         | 12        | 0.07                   | <b>22.4</b>                | 1.19            | 1.59            | 1.96             | 0.2 | 0.07  | 0.0  | <b>0.15</b>                                  | 0.21   | <b>0.26</b>                                    | 12               | 0.0050 | 12  | <b>2.19</b>  | 2.8 | 0.015                | 0.0000 |     |          |          |  |
| S5         | S4   | DI-S4AE&DI-S4AW     | 0.00            | <b>1.00</b>  |                          |                            | 2.8         | 105       | 0.63                   | <b>25.7</b>                | 1.06            | 1.49            | 1.83             | 0.2 | 0.50  | 0.1  | <b>0.96</b>                                  | 1.39   | <b>1.73</b>                                    | 12               | 0.0050 | 105 | <b>2.19</b>  | 2.8 | 0.015                | 0.0010 |     |          |          |  |
| S4         | S3   | S5&S4A              | 0.00            | <b>1.00</b>  |                          |                            | 3.9         | 155       | 0.66                   | <b>23.0</b>                | 1.16            | 1.57            | 1.93             | 0.2 | 0.50  | 0.1  | <b>1.06</b>                                  | 1.47   | <b>1.83</b>                                    | 12               | 0.0100 | 155 | <b>3.09</b>  | 3.9 | 0.015                | 0.0012 |     |          |          |  |
| S3         | S2   | S4                  | 0.00            | <b>1.00</b>  |                          |                            | 3.9         | 330       | 1.40                   | <b>27.1</b>                | 1.01            | 1.45            | 1.78             | 0.2 | 0.50  | 0.1  | <b>0.91</b>                                  | 1.35   | <b>1.68</b>                                    | 12               | 0.0100 | 330 | <b>3.09</b>  | 3.9 | 0.015                | 0.0009 |     |          |          |  |
| S2         | S1   | S3                  | 0.00            | <b>1.00</b>  |                          |                            | 3.9         | 365       | 1.55                   | <b>24.6</b>                | 1.10            | 1.52            | 1.87             | 0.2 | 0.50  | 0.1  | <b>1.00</b>                                  | 1.42   | <b>1.77</b>                                    | 12               | 0.0100 | 365 | <b>3.09</b>  | 3.9 | 0.015                | 0.0010 |     |          |          |  |
| S1         | SOUT | M1, S2&DI-S1N       | 0.81            | <b>11.73</b> |                          |                            | 8.2         | 45        | 0.09                   | <b>27.2</b>                | 1.00            | 1.45            | 1.78             | 0.2 | 5.87  | 1.2  | <b>10.61</b>                                 | 15.78  | <b>19.69</b>                                   | 36               | 0.0100 | 45  | <b>57.93</b> | 8.2 | 0.015                | 0.0003 |     |          |          |  |
| SOUT       |      |                     |                 |              |                          |                            |             |           |                        |                            |                 |                 |                  |     |       |      |  |  |  |                  |        |     |              |     |                      |        |     |          |          |  |
| WEST SHED  |      |                     |                 |              |                          |                            |             |           |                        |                            |                 |                 |                  |     |       |      |  |  |  |                  |        |     |              |     |                      |        |     |          |          |  |
| DI-W5N     | W5   | OVERLAND            | 0.78            | <b>0.78</b>  | 15.00                    | 5.68                       | 2.8         | 12        | 0.07                   | <b>20.7</b>                | 1.28            | 1.66            | 2.04             | 0.2 | 0.39  | 0.1  | <b>0.92</b>                                  | 1.22   | <b>1.51</b>                                    | 12               | 0.0050 | 12  | <b>2.19</b>  | 2.8 | 0.015                | 0.0009 |     |          |          |  |
| DIW5S      | W5   | OVERLAND            | 0.78            | <b>0.78</b>  | 15.00                    | 5.24                       | 2.8         | 24        | 0.14                   | <b>20.2</b>                | 1.30            | 1.68            | 2.06             | 0.2 | 0.39  | 0.1  | <b>0.94</b>                                  | 1.23   | <b>1.53</b>                                    | 12               | 0.0050 | 24  | <b>2.19</b>  | 2.8 | 0.015                | 0.0009 |     |          |          |  |
| W5         | W4   | DI-W5N&DI-W5S       | 0.00            | <b>1.56</b>  |                          |                            | 2.8         | 100       | 0.60                   | <b>21.3</b>                | 1.24            | 1.63            | 2.01             | 0.2 | 0.78  | 0.2  | <b>1.79</b>                                  | 2.39   | <b>2.98</b>                                    | 12               | 0.0050 | 100 | <b>2.19</b>  | 2.8 | 0.015                | 0.0033 |     |          |          |  |
| W4         | W3   | W4, W4A&DI-W4W      | 0.72            | <b>2.28</b>  |                          |                            | 3.6         | 245       | 1.12                   | <b>22.4</b>                | 1.19            | 1.59            | 1.96             | 0.2 | 1.14  | 0.2  | <b>2.49</b>                                  | 3.40   | <b>4.24</b>                                    | 18               | 0.0050 | 245 | <b>6.45</b>  | 3.6 | 0.015                | 0.0007 |     |          |          |  |
| W3         | W2   | W3&DI-W3S           | 0.61            | <b>2.89</b>  |                          |                            | 3.6         | 120       | 0.55                   | <b>23.0</b>                | 1.17            | 1.57            | 1.94             | 0.2 | 1.45  | 0.3  | <b>3.08</b>                                  | 4.26   | <b>5.31</b>                                    | 18               | 0.0050 | 120 | <b>6.45</b>  | 3.6 | 0.015                | 0.0011 |     |          |          |  |
| W2         | W1   | W2, DI-W2N&DI-W3S   | 1.82            | <b>4.71</b>  |                          |                            | 4.4         | 150       | 0.57                   | <b>23.5</b>                | 1.14            | 1.55            | 1.91             | 0.2 | 2.36  | 0.5  | <b>4.90</b>                                  | 6.85   | <b>8.54</b>                                    | 24               | 0.0050 | 150 | <b>13.89</b> | 4.4 | 0.015                | 0.0006 |     |          |          |  |
| W1         |      |                     |                 |              |                          |                            |             |           |                        |                            |                 |                 |                  |     |       |      |  |  |  |                  |        |     |              |     |                      |        |     |          |          |  |

\* From Fig. 5-1 Placer County Drainage Manual

\*\* From Fig. 5-2 Placer County Drainage Manual

**APPENDIX C**

Form D-1e  
LID Worksheets

**Appendix D-1: Residential Sites: Runoff Reduction Credits and Treatment BMP Sizing Calculations**

Name of Drainage Shed:  Fill in Highlighted Boxes  
 Project Located in

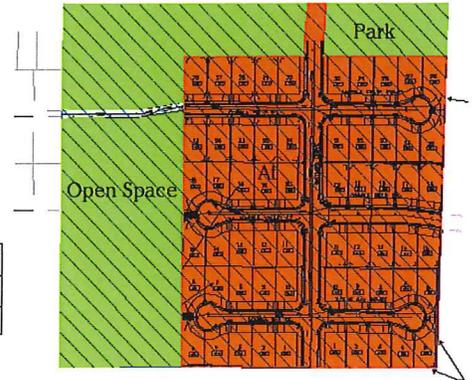
**Step 1 - Calculate Area Requiring Treatment**

|   |   |                 |                               |
|---|---|-----------------|-------------------------------|
| Drainage Shed Area  | <input type="text" value="24.8"/> acres                 | A               | <b>See Area Example Below</b> |
| Open Space and Parks Acreage*                                       | <input type="text" value="4.2"/>                        | A <sub>OS</sub> |                               |
| Treatment Area  | A - A <sub>OS</sub> = <input type="text" value="20.6"/> | A <sub>T</sub>  |                               |
| Number of Units in A <sub>T</sub>                                   | <input type="text" value="100"/>                        |                 |                               |
| Number of units per acre in A <sub>T</sub>                          | DUA/A <sub>T</sub> = <input type="text" value="5"/>     |                 |                               |
| Assumed Initial Impervious Fraction<br>(determine using Table D-1a) | <input type="text" value="0.35"/>                       | I               |                               |

\*. Includes all areas maintained in a natural state and planned for landscaped park areas

| Dwelling units per acre | Imperviousness |
|-------------------------|----------------|
| 1                       | 0.17           |
| 2                       | 0.25           |
| 3,4                     | 0.35           |
| 5,6                     | 0.40           |
| 7                       | 0.50           |
| 8,9                     | 0.55           |
| 10-14                   | 0.60           |
| 15-20                   | 0.70           |

|  |   |
|--|---|
|  | <b>A - Drainage Shed Area</b>                               |
|  | <b>A<sub>OS</sub> - Parks and Open Space</b>                |
|  | <b>A<sub>T</sub> - Area with Runoff Reduction Potential</b> |



**Step 2 - Calculate Impervious Area Treatments**

| Runoff Reduction Measures                         | Effective Area Managed (A <sub>C</sub> )  |
|---|---|
| Disconnected Roof Drains<br>(see Fact Sheet)      | use Form D-1a for credits → <input type="text" value="3.52"/> acres                                 |
| Disconnected Pavement<br>(see Fact Sheet)         | use Form D-1b for credits → <input type="text" value="0.77"/> acres                                 |
| Interceptor Trees<br>(see Fact Sheet)             | use Form D-1c for credits → <input type="text" value="0.69"/> acres                                 |
| Alternative Driveway Design<br>(see Fact Sheet)   | use Form D-1d for credits → <input type="text" value="0.00"/> acres                                 |
| <b>Total Effective Area Managed (Credit Area)</b> | <b>A<sub>C</sub></b> <input type="text" value="4.98"/> acres  |
| <b>Adjusted Area for Flow-Based Treatment</b>     | A <sub>T</sub> - A <sub>C</sub> = <input type="text" value="15.57"/> acres <b>A<sub>AT</sub></b>    |
| <b>Adjusted Impervious Fraction for A</b>         | (A <sub>T</sub> (I) - A <sub>C</sub> ) / A = <input type="text" value="0.09"/> <b>I<sub>A</sub></b> |

**Form D-1a: Disconnected Roof Drains Worksheet**

See Fact Sheet for more information regarding Disconnected Roof Drain credit guidelines

Effective Area Managed (A<sub>c</sub>)**1. Determine efficiency Multiplier**

|   |                   |      |
|---|-------------------|------|
| Runoff is directed to a dispersal trench or dry well<br>(Type A and B soils only) |                   | 1.00 |
| Runoff is directed across landscaping, determine setback                          |                   |      |
| 25 ft +   | Use multiplier of | 1.00 |
| ≥ 20 and < 25 ft  | Use multiplier of | 0.90 |
| ≥ 15 and < 20 ft  | Use multiplier of | 0.70 |
| ≥ 10 and < 15 ft  | Use multiplier of | 0.45 |
| ≥ 5 and < 10 ft   | Use multiplier of | 0.25 |

Efficiency Multiplier

0.90

Box J1

**2. Determine percentage of roof drains disconnected**

100.0%

Box J2

**3. Select project density in dwelling units per acre:**

|       |                         |      |
|-------|-------------------------|------|
| 1     | Use reduction factor of | 0.08 |
| 2     | Use reduction factor of | 0.13 |
| 3,4   | Use reduction factor of | 0.19 |
| 5,6   | Use reduction factor of | 0.23 |
| 7     | Use reduction factor of | 0.29 |
| 8,9   | Use reduction factor of | 0.33 |
| 10-14 | Use reduction factor of | 0.37 |
| 15-20 | Use reduction factor of | 0.44 |

Reduction Factor

0.19

Box J3

**4. Determine Area Managed**Multiply Box J3 by A<sub>T</sub>, and enter the result in Box J4

3.9 acres

Box J4

**5. Multiply Boxes J1, J2 and J4, and enter the Result in Box J**

3.5 acre: Box J

This is the amount of area credit to enter into the "Disconnected Roof Drains" Box of Form D-1

**Form D-1b: Disconnected Pavement Worksheet**

See Fact Sheet for more information regarding NDC Pavement credit guidelines

Effective Area Managed (A<sub>c</sub>)**Divided Sidewalks****1. Determine percentage of units with divided Sidewalks**

94.0%

Box K1

Multiply Box K1, A<sub>T</sub>, and 0.04 and enter the result in Box K

0.77 acre: Box K

This is the amount of area credit to enter into the "Disconnected Pavement" Box of Form D-1

**Form D-1c: Interceptor Tree Worksheet**

See Fact Sheet for more information regarding Interceptor Tree credit guidelines

Effective Area Managed (A<sub>c</sub>)**New Evergreen Trees****1. Enter number of new evergreen trees that qualify as Interceptor Trees in Box L1.**

100

trees

Box L1

**2. Multiply Box L1 by 200 and enter result in Box L2**

20000

sq. ft.

Box L2

**New Deciduous Trees****3. Enter number of new deciduous trees that qualify as Interceptor Trees in Box L3.**

100

trees

Box L3

**4. Multiply Box L3 by 100 and enter result in Box L4**

10000

sq. ft.

Box L4

**Existing Tree Canopy****5. Enter square footage of existing tree canopy that qualifies as Existing Tree canopy in Box L5.**

0

sq. ft.

Box L5

**6. Multiply Box L5 by 0.5 and enter the result in Box L6**

0

sq. ft.

Box L6

**Total Interceptor Tree Credits**

Add Boxes L2, L4, and L6 and enter it into Box L7

30000

sq. ft.

Box L7

Divide Box L7 by 43,560 to get the number of acres effectively managed and enter the result in Box L8

0.69

acres

Box L8

This is the amount of area credit to enter into the "Interceptor Trees" Box of Form D-1

### Form D-1d: Alternative Driveway Design

See Fact Sheet for more information regarding Alternative Driveway Design credit guidelines

1. Select type of driveway

| Pervious Driveway:  | Multiplier: |
|---|-------------|
| Cobblestone Block Porous Pavement   | 0.40        |
| Pervious Concrete/Asphalt Pavement  | 0.60        |
| Modular Block Porous Pavement<br>Porous Gravel Pavement &<br>Hollywood Driveway | 0.75        |
| Not Directly-connected Driveway   | 1.00        |

Box M1

2. Determine percentage of units with Alternative Driveways:

Box M2

4. Multiply Boxes M1, M2, A<sub>T</sub> and 0.04, and enter the result in Box M

This is the amount of area credit to enter into the "Alternative Driveway Design" Box of Form D-1

acres Box M

### Step 3 - Calculate Flow or Volume Requiring Treatment

#### Form D-1e Treatment - Flow-Based (Rational Method)

Calculate treatment flow (cfs):

$$\text{Flow} = \text{Runoff Coefficient} \times \text{Rainfall Intensity} \times \text{Adjusted Treatment Area}$$

Determine C Factor using Table D-1b

C

Determine i using Table D-1c (Rainfall Intensity)

i

A<sub>AT</sub> from Step 2

A<sub>AT</sub>

$$\text{Flow} = C \times i \times A_{AT}$$

cfs

TABLE D-1b

| Runoff Coefficient (Rational), C |      |
|----------------------------------|------|
| Single-family areas              | 0.50 |
| Multi-units, detached            | 0.60 |
| Apartment dwelling areas         | 0.70 |
| Multi-units, attached            | 0.75 |
| User Specified                   | 0.00 |

Table D-1c

| Rainfall Intensity |     |      |       |
|--------------------|-----|------|-------|
| Roseville          | i = | 0.20 | in/hr |
| Sacramento         | i = | 0.18 | in/hr |
| Folsom             | i = | 0.20 | in/hr |

#### Form D-1f Treatment - Volume-Based (CASQA)

[use this method for Roseville Volume Calculations](#)

Calculate treatment volume (Acre-Feet):

$$\text{Treatment Volume} = \text{Area} \times (\text{Storage Volume} + \text{Conversion Factor})$$

Determine Adjusted C<sub>A</sub> using Table D-2d (for CASQA Method) and the Adjusted Impervious Fraction (I<sub>A</sub>) from Step 2

C<sub>A</sub>

hrs Specified Draw Down time

Determine Unit Basin Storage Volume (Fig. D-2A) using C<sub>A</sub>

SV

A from Step 1

A

$$\text{Treatment volume} = A_T \times (SV / 12)$$

Acre-Feet

#### Form D-1g Treatment - Volume-Based (ASCE-WEF)

Calculate water quality volume (Acre-Feet):

$$\text{WQV} = \text{Area} \times \text{Maximized Detention Volume (P}_0\text{)}$$

A from Step 1

A

hrs Specified Draw Down time

Obtain P<sub>0</sub>: Maximized Detention Volume from figures E-1 to E-4 in Appendix E of this manual using I<sub>A</sub> from Step 2.

P<sub>0</sub>

$$\text{Treatment volume} = A \times (P_0 / 12)$$

Acre-Feet

**Appendix D-1: Residential Sites: Runoff Reduction Credits and Treatment BMP Sizing Calculations**

Name of Drainage Shed:  Fill in Highlighted Boxes  
 Project Located in

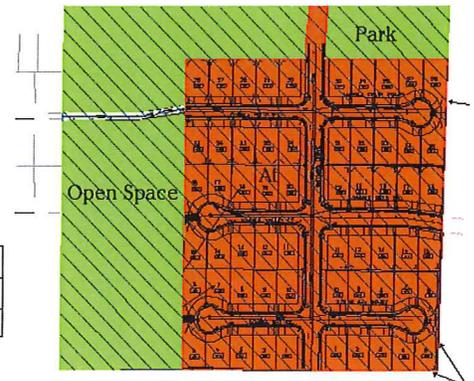
**Step 1 - Calculate Area Requiring Treatment**

|   |   |                 |                               |
|---|---|-----------------|-------------------------------|
| Drainage Shed Area  | <input type="text" value="15.3"/> acres                 | A               |                               |
| Open Space and Parks Acreage*                                       | <input type="text" value="3.5"/>                        | A <sub>OS</sub> |                               |
| Treatment Area  | A - A <sub>OS</sub> = <input type="text" value="11.8"/> | A <sub>T</sub>  | <b>See Area Example Below</b> |
| Number of Units in A <sub>T</sub>                                   | <input type="text" value="48"/>                         |                 |                               |
| Number of units per acre in A <sub>T</sub>                          | DU/A <sub>T</sub> = <input type="text" value="4"/>      |                 |                               |
| Assumed Initial Impervious Fraction<br>(determine using Table D-1a) | <input type="text" value="0.35"/>                       | I               |                               |

\*. Includes all areas maintained in a natural state and planned for landscaped park areas

| Dwelling units per acre | Imperviousness |
|-------------------------|----------------|
| 1                       | 0.17           |
| 2                       | 0.25           |
| 3,4                     | 0.35           |
| 5,6                     | 0.40           |
| 7                       | 0.50           |
| 8,9                     | 0.55           |
| 10-14                   | 0.60           |
| 15-20                   | 0.70           |

|  |   |
|--|---|
|  | <b>A - Drainage Shed Area</b>                               |
|  | <b>A<sub>OS</sub> - Parks and Open Space</b>                |
|  | <b>A<sub>T</sub> - Area with Runoff Reduction Potential</b> |



**Step 2 - Calculate Impervious Area Treatments**

| Runoff Reduction Measures                         |  | Effective Area Managed (A <sub>C</sub> )                     |
|---|--|--|
| Disconnected Roof Drains<br>(see Fact Sheet)      | use Form D-1a for credits  | <input type="text" value="2.01"/> acres                      |
| Disconnected Pavement<br>(see Fact Sheet)         | use Form D-1b for credits  | <input type="text" value="0.42"/> acres                      |
| Interceptor Trees<br>(see Fact Sheet)             | use Form D-1c for credits  | <input type="text" value="0.33"/> acres                      |
| Alternative Driveway Design<br>(see Fact Sheet)   | use Form D-1d for credits  | <input type="text" value="0.00"/> acres                      |
| <b>Total Effective Area Managed (Credit Area)</b> |  | <b>A<sub>C</sub></b> <input type="text" value="2.77"/> acres |
| <b>Adjusted Area for Flow-Based Treatment</b>     | A <sub>T</sub> - A <sub>C</sub> = <input type="text" value="8.98"/> acres      | <b>A<sub>AT</sub></b>  |
| <b>Adjusted Impervious Fraction for A</b>         | (A <sub>T</sub> (I) - A <sub>C</sub> ) / A = <input type="text" value="0.09"/> | <b>I<sub>A</sub></b>   |

### Form D-1a: Disconnected Roof Drains Worksheet

See Fact Sheet for more information regarding Disconnected Roof Drain credit guidelines

Effective Area Managed (A<sub>c</sub>)

#### 1. Determine efficiency Multiplier

|   |                        |
|---|------------------------|
| Runoff is directed to a dispersal trench or dry well<br>(Type A and B soils only) | 1.00                   |
| Runoff is directed across landscaping, determine setback                          |                        |
| 25 ft +   | Use multiplier of 1.00 |
| ≥ 20 and < 25 ft  | Use multiplier of 0.90 |
| ≥ 15 and < 20 ft  | Use multiplier of 0.70 |
| ≥ 10 and < 15 ft  | Use multiplier of 0.45 |
| ≥ 5 and < 10 ft   | Use multiplier of 0.25 |

Efficiency Multiplier →  Box J1

#### 2. Determine percentage of roof drains disconnected

→  Box J2

#### 3. Select project density in dwelling units per acre:

|       |                         |      |
|-------|-------------------------|------|
| 1     | Use reduction factor of | 0.08 |
| 2     | Use reduction factor of | 0.13 |
| 3,4   | Use reduction factor of | 0.19 |
| 5,6   | Use reduction factor of | 0.23 |
| 7     | Use reduction factor of | 0.29 |
| 8,9   | Use reduction factor of | 0.33 |
| 10-14 | Use reduction factor of | 0.37 |
| 15-20 | Use reduction factor of | 0.44 |

Reduction Factor →  Box J3

#### 4. Determine Area Managed

Multiply Box J3 by A<sub>T</sub>, and enter the result in Box J4  acres Box J4

#### 5. Multiply Boxes J1, J2 and J4, and enter the Result in Box J

acre: Box J

This is the amount of area credit to enter into the "Disconnected Roof Drains" Box of Form D-1

### Form D-1b: Disconnected Pavement Worksheet

See Fact Sheet for more information regarding NDC Pavement credit guidelines

Effective Area Managed (A<sub>c</sub>)

#### Divided Sidewalks

#### 1. Determine percentage of units with divided Sidewalks

Box K1

Multiply Box K1, A<sub>T</sub>, and 0.04 and enter the result in Box K

acre: Box K

This is the amount of area credit to enter into the "Disconnected Pavement" Box of Form D-1

### Form D-1c: Interceptor Tree Worksheet

See Fact Sheet for more information regarding Interceptor Tree credit guidelines

Effective Area Managed (A<sub>c</sub>)

#### New Evergreen Trees

#### 1. Enter number of new evergreen trees that qualify as Interceptor Trees in Box L1.

trees Box L1

#### 2. Multiply Box L1 by 200 and enter result in Box L2

sq. ft. Box L2

#### New Deciduous Trees

#### 3. Enter number of new deciduous trees that qualify as Interceptor Trees in Box L3.

trees Box L3

#### 4. Multiply Box L3 by 100 and enter result in Box L4

sq. ft. Box L4

#### Existing Tree Canopy

#### 5. Enter square footage of existing tree canopy that qualifies as Existing Tree canopy in Box L5.

sq. ft. Box L5

#### 6. Multiply Box L5 by 0.5 and enter the result in Box L6

sq. ft. Box L6

#### Total Interceptor Tree Credits

Add Boxes L2, L4, and L6 and enter it into Box L7

sq. ft. Box L7

Divide Box L7 by 43,560 to get the number of acres effectively managed and enter the result in Box L8

acres Box L8

This is the amount of area credit to enter into the "Interceptor Trees" Box of Form D-1

### Form D-1d: Alternative Driveway Design

See Fact Sheet for more information regarding Alternative Driveway Design credit guidelines

1. Select type of driveway

| Pervious Driveway:  | Multiplier: |
|---|-------------|
| Cobblestone Block Porous Pavement   | 0.40        |
| Pervious Concrete/Asphalt Pavement  | 0.60        |
| Modular Block Porous Pavement<br>Porous Gravel Pavement &<br>Hollywood Driveway | 0.75        |
| Not Directly-connected Driveway   | 1.00        |

Box M1

2. Determine percentage of units with Alternative Driveways:

Box M2

4. Multiply Boxes M1, M2, A<sub>T</sub> and 0.04, and enter the result in Box M

This is the amount of area credit to enter into the "Alternative Driveway Design" Box of Form D-1

acres Box M

### Step 3 - Calculate Flow or Volume Requiring Treatment

#### Form D-1e Treatment - Flow-Based (Rational Method)

Calculate treatment flow (cfs):

$$\text{Flow} = \text{Runoff Coefficient} \times \text{Rainfall Intensity} \times \text{Adjusted Treatment Area}$$

Determine C Factor using Table D-1b

C

Determine i using Table D-1c (Rainfall Intensity)

i

A<sub>AT</sub> from Step 2

A<sub>AT</sub>

$$\text{Flow} = C \times i \times A_{AT}$$

cfs

TABLE D-1b

| Runoff Coefficient (Rational), C |      |
|----------------------------------|------|
| Single-family areas              | 0.50 |
| Multi-units, detached            | 0.60 |
| Apartment dwelling areas         | 0.70 |
| Multi-units, attached            | 0.75 |
| User Specified                   | 0.00 |

Table D-1c

| Rainfall Intensity |     |      |       |
|--------------------|-----|------|-------|
| Roseville          | i = | 0.20 | in/hr |
| Sacramento         | i = | 0.18 | in/hr |
| Folsom             | i = | 0.20 | in/hr |

#### Form D-1f Treatment - Volume-Based (CASQA)

[use this method for Roseville Volume Calculations](#)

Calculate treatment volume (Acre-Feet):

$$\text{Treatment Volume} = \text{Area} \times (\text{Storage Volume} + \text{Conversion Factor})$$

Determine Adjusted C<sub>A</sub> using Table D-2d (for CASQA Method) and the Adjusted Impervious Fraction (I<sub>A</sub>) from Step 2

C<sub>A</sub>

hrs Specified Draw Down time

Determine Unit Basin Storage Volume (Fig. D-2A) using C<sub>A</sub>

SV

A from Step 1

A

$$\text{Treatment volume} = A_T \times (SV / 12)$$

Acre-Feet

#### Form D-1g Treatment - Volume-Based (ASCE-WEF)

Calculate water quality volume (Acre-Feet):

$$\text{WQV} = \text{Area} \times \text{Maximized Detention Volume (P}_0\text{)}$$

A from Step 1

A

hrs Specified Draw Down time

Obtain P<sub>0</sub>: Maximized Detention Volume from figures E-1 to E-4 in Appendix E of this manual using I<sub>A</sub> from Step 2.

P<sub>0</sub>

$$\text{Treatment volume} = A \times (P_0 / 12)$$

Acre-Feet

## **APPENDIX D**

### Detention Basins